

## Description

Piezoelectric Ceramic Material, Multilayer Component  
and Method for Producing Said Ceramic Material

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The invention relates to a piezoelectric ceramic material having the general composition  $ABO_3$ , which essentially contains lead zirconate titanate and has a perovskite lattice structure, in which A stands for A positions and B stands for B positions in the crystal lattice. The invention further relates to a method for producing this ceramic material.

This type of ceramic material is especially well suited for use in multilayer components comprising a stack of multiple ceramic layers and electrode layers arranged alternately, one on top of another.

Piezoceramic components of this type can be used, for example, as actuators in piezo stacks, in which a low-inertia mechanical deflection of comparatively high force is achieved by means of voltage activation; they may also allow the generation of high electric voltages or may be used in relevant devices in the detection of mechanical oscillations or the generation of acoustic vibrations.

Prior technical solutions have been based predominantly on ceramic masses of the perovskite structural type having the general formula  $ABO_3$ , wherein the piezoelectric properties are brought to bear in the ferroelectric state. Lead zirconate titanate ceramics that

have been modified using select additives,  $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3 =$   
PZT, the composition of which is tailored to the so-called  
morphotropic phase boundary of two coexisting ferroelectric  
phases, have proven particularly advantageous. Between the  
5 ceramic layers, which are produced according to methods  
customarily used with ceramics, especially ceramic foil  
technology, precious metal internal electrodes, for example  
Ag/Pd in a 70/30 molar ratio, are applied by means of the  
screen printing process. With up to several hundred  
10 electrode layers per component, these components are  
burdened with substantial costs. The precious metal  
electrodes enable the thermal elimination, in air, of  
dispersants and binders and other organic additives, along  
with the organic components of the screen printing metal  
15 paste, from the multilayer stacks by means of  
depolymerization and oxidation, thus enabling a subsequent  
sinter densification at ca. 1100 to 1150° C without  
reduction effects that could, for example, be caused by  
residual carbon, which would negatively influence the  
20 properties of the ceramic as a result of reduction  
reactions.

In the publication DE 20023051 U1 a method for  
producing piezoelectric components is disclosed, which uses  
25 copper-containing electrodes in place of the costly Ag/Pd  
internal electrodes, wherein the piezoelectric ratings are  
based upon ceramic masses having the preferred composition  
 $\text{Pb}_{0.97}\text{Nd}_{0.02}\square_{0.01}(\text{Zr}_{0.54}\text{Ti}_{0.46})\text{O}_3$ . The symbol " $\square$ " stands for a  
vacancy in the crystal lattice. Ceramic masses having this  
30 type of composition are particularly well suited for use in  
Ag/Pd internal electrodes and for air sintering at 1120° C,

and are tailored with respect to their piezoelectric properties such that they partially take up silver from the internal electrodes. The acquisition of the silver is made possible by the presence of atmospheric oxygen during the sintering process. At the same time, grain growth is promoted, so that in the finished component a ceramic composition  $\text{Pb}_{0.96}\text{Nd}_{0.02}\text{Ag}_{0.02}(\text{Zr}_{0.54}\text{Ti}_{0.46})\text{O}_3$  results, with a grain structure that is favorable for the intended application.

In contrast, the multilayer piezoelectric components that have the same initial composition as the ceramic and copper-containing internal electrodes do not have this type of silver content, with the result that the morphotropic phase boundary that is advantageous for optimal piezoelectric properties is no longer present in the ceramic, and the average grain size is smaller. The latter is primarily also a result of the lower sintering temperature of ca. 1000° C, which must be maintained when internal electrodes containing copper are used, in order to prevent a melting of the electrodes.

Although, with the sintering of multilayer components based upon the PZT ceramic of the composition  $\text{Pb}_{0.97}\text{Nd}_{0.02}\text{□}_{0.01}(\text{Zr}_{0.54}\text{Ti}_{0.46})\text{O}_3$  with Ag/Pd internal electrodes in an air atmosphere at 1120° C, the silver becomes inserted evenly over the entire cross-section of the sintered ceramic layer, so that the composition  $\text{Pb}_{0.96}\text{Nd}_{0.02}\text{Ag}_{0.02}(\text{Zr}_{0.54}\text{Ti}_{0.46})\text{O}_3$  is established in the piezoceramic, with the sintering of a multilayer ceramic component that has copper-containing internal electrodes

the copper content in ceramic layers having the above-named composition amounts to only ca. 0.1 m%.

The deviation from the morphotropic phase boundary is perceived for example in a lower dielectric constant  $\epsilon$  and in an increase in the temperature coefficient  $TK\epsilon$  of the DK (measured, for example, between  $-20^{\circ}\text{C}$  and  $60^{\circ}\text{C}$ , ascending) and also in a lower degree of deflection  $S_3$  at the same field intensity  $E_3$  ( $DK$  = dielectric constant).

The deflection parameter  $d_{33}$  (= piezoelectric charge constant) is defined by the equation  $S_3 = d_{33} \cdot E_3$ . Furthermore, in the assessment of the suitability of a piezoceramic for use in multilayer components the dielectric loss  $L$  is the critical factor, which, as a function of the electric activation, causes a more or less significant temperature increase in the component and can be described using the degree of efficiency  $\eta = E_a/E_e$  ( $E_a$  = energy that can be coupled out,  $E_e$  = coupled-in energy) combined with the electric field intensity that is associated with a certain degree of deflection  $E = U/d$  ( $d$  = thickness of the ceramic layer), by means of the equation  $L = (1/2)U^2C(1 - \eta)$  ( $C$  = capacitance).

The object of the invention is to disclose a ceramic material of the above-described type that is especially well suited for use in multilayer ceramic components, and which will ensure a diminished dielectric loss  $L$  thus ensuring a low temperature increase in the multilayer

components over long-term use while at the same time  
ensuring adequate deflection  $S_3$ .

The object of the invention is attained with a  
5 piezoelectric ceramic material of the type described at the  
beginning, having the characterizing features disclosed in  
claim 1.

The ceramic material of the invention is characterized  
10 by a composition that contains at least a proportion of  
lead zirconate titanate of the general formula  $Pb_{1-3x/2-y/2}SE_x□_{x/2-y/2}Cu^I_y(Zr_{0.5515-z}Ti_{0.4485+z})O_3$ , wherein  $0.01 < x < 0.04$   
and  $0 < y < x/2$ . The parameter  $z$  can have any value  
between  $-0.15 < z < +0.15$ , preferably  $-0.016 < z < 0.0205$ .  
15 SE stands for a rare-earth metal, selected from the group  
La, Nd, Sm, Gd, Tb, Dy, Ho, Er, Tu, Yb, Lu and Y. The  
parameter  $x$  is determined by the valence of the rare-earth  
metal. The ratio Zr/Ti given by the parameter  $z$  is  
selected based upon the copper content, i.e. upon the  
20 parameter  $y$ , such that the ceramic material is tailored in  
terms of its phase state (in the phase state diagram) to  
the morphotropic phase boundary.

In the context of the invention the phase boundary is  
25 not necessarily narrowly defined, rather in the phase state  
diagram it can correspond to a morphotropic phase range,  
for example between two defined crystal modifications.

According to the invention, the insertion of the  
30 divalent  $Cu^{2+}$  cation in the B positions of the ceramic  
lattice is prevented for the reasons enumerated below.

Even after sintering of the ceramic mass the copper remains monovalent.

As a result of the insertion of  $\text{Cu}^+$  cations in A  
5 positions in the ceramic lattice structure, in terms of the physical properties especially the reduction in dielectric losses L in the ceramic material is achieved, see Table 5.

One advantageous modification in the body composition  
10 of the piezoceramic results, for example, from changing the molar ratio Zr/Ti by varying the parameter z according to the formula  $\text{Pb}_{1-3x/2}\text{Se}_{x/2}(\text{Zr}_{0.5515-z}\text{Ti}_{0.4485+z})\text{O}_3$  to the point at which the morphotropic phase boundary is also reached in the ceramic, which is formed as a result of sintering at  
15 ca.  $1000^\circ\text{C}$  under inert conditions in the presence of Cu internal electrodes, in other words without the insertion of silver. In this manner particularly favorable piezoelectric properties for the ceramic can be obtained.

20 In another variant it is advantageous to tailor the composition of the ceramic material to the copper-containing internal electrodes by adding a select amount of copper oxide to the ceramic mass - varying the parameter y according to the general formula  $\text{Pb}_{1-3x/2-y/2}\text{Se}_{x/2-y/2}\text{Cu}_y(\text{Zr}_{0.5515-z}\text{Ti}_{0.4485+z})\text{O}_3$ , wherein  $0.01 < x < 0.04$  and  $0 < y < x/2$ .

If a certain amount of CuO is added to the starting material mixture with a PZT mass stock of a certain  
30 composition, it can be assumed that in the subsequent calcination in air an insertion of  $\text{Cu}^{2+}$  ions in the

perovskite lattice structure of the ceramic will occur, wherein  $\text{Cu}^{2+}$  as an acceptor prefers to occupy B positions, so that as a result of the calcination, assuming a complete conversion, the formula  $\text{Pb}_{1-3x/2}\text{SE}_x\text{O}_{x/2}[(\text{Zr}_{0.5515-z}\text{Ti}_{0.4485+z})]_{1-y}\text{Cu}^{\text{II}}_y\text{O}_{3-y}\text{O}_y$  will result. However under the conditions of a combined sintering with copper-containing internal electrodes,  $\text{Cu}^{2+}$  is not stable.  $\text{Cu}^+$  ions form and, due to their large ionic radius, prefer to occupy A positions in the perovskite structure.

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Accordingly, the sintered ceramic is allocated a composition according to the formula  $\text{Pb}_{1-3x/2-y/2}\text{SE}_x\text{O}_{x/2-y/2}\text{Cu}_y(\text{Zr}_{0.5515-z}\text{Ti}_{0.4485+z})\text{O}_3$  with  $\text{Cu}^+$  ions in A positions, for example in the case of  $y = x$  with  $\text{Pb}_{1-3x/2}\text{SE}_x\text{Cu}^{\text{I}}_x(\text{Zr}_{0.5515-z}\text{Ti}_{0.4485+z})\text{O}_3$ . The vacant oxygen positions, which are formed as a result of the insertion of  $\text{Cu}^{2+}$  in B positions, are no longer present due to the alteration of the lattice during sintering as a result of  $\text{Cu}^+$  formation. Once the maximum Cu content (for the given SE cation) has been reached, the Cu, which was added in the form of a copper oxide, will no longer be taken up by the perovskite lattice.

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To avoid the insertion of  $\text{Cu}^{2+}$  ions in B positions, the mass stock of a relevant composition is advantageously first converted without the addition of  $\text{CuO}$ , after which the copper oxide is added to the slurry as  $\text{Cu}_2\text{O}$ , so that the insertion into the A positions of the perovskite lattice structure can take place immediately following a successful debinding of the multilayer piezoelectric component during the sintering process.

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The invention will be described in greater detail below with reference to an exemplary embodiment.

A raw materials mixture comprised of

- 5           1)  $\text{TiO}_2$ ,  $\text{ZrO}_2$  or a precursor  $(\text{Zr}, \text{Ti})\text{O}_2$  produced  
via mixture precipitation,  
          2)  $\text{PbCO}_3$  or  $\text{Pb}_3\text{O}_4$ ,  
          3) Doping agents from an oxide of a rare-earth  
metal, for example  $\text{Nd}_2\text{O}_3$ , and  
10          4) An admixture of  $\text{CuO}$

is weighed in with a) a composition that corresponds to or approaches the morphotropic phase boundary and b) a  $\text{PbO}$  surplus of a maximum of 5% for the purpose of promoting sinter densification. This mixture is subjected to a  
15 grinding stage to promote equidistribution of the components in an aqueous suspension, and after filtering and drying, for example at 900 to 950° C in an air atmosphere, is calcined.

20          In a further advantageous variant, the copper oxide is not added in the calcination stage. The calcination results in the formation of a piezoceramic perovskite mixed crystal phase.

25          To achieve a sinter densification of the ceramic mass at only 1000° C, i.e. below the melting point of copper, within 2 to 8 hours, the ceramic powder is finely ground to an average grain size of  $< 0.4 \mu\text{m}$ . The sinter activity of the powder then proves to be sufficient to produce a  
30 ceramic density of greater than 97% of the theoretic



density, with simultaneously adequate grain growth and sufficient mechanical strength in the grain structure.

The finely ground ceramic powder is suspended using a  
5 dispersant to an aqueous slurry with an approximately 70 m%  
(= mass percent) solids content, which corresponds to  
approximately 24 vol-%. In this, the proportion of  
dispersant, for example ammonium citrate, that is required  
for an optimal dispersion is specifically determined  
10 through a series of experiments, and can be identified with  
the achievement of a minimum viscosity. In the case of the  
production of a ceramic that contains copper oxide from a  
conversion powder, to which no copper oxide was added prior  
to calcination, a certain amount of the copper(I) oxide  $\text{Cu}_2\text{O}$   
15 is added. For the formation of the piezoceramic green  
film, approximately 6 m% of a commercial,  
thermohydrolytically degradable binding agent is added to  
the dispersed solid powder suspensions. An aqueous  
polyurethane dispersion has proven advantageous for this  
20 purpose. This is mixed, for example, in a Dispermat  
grinder, which results in a slurry that is suitable for the  
film extrusion process.

The debinding is then performed thermohydrolytically  
25 using water vapor in a nitrogen atmosphere. The hydrolytic  
separation of the binder occurs for the most part at a  
relatively low temperature of  $220 \pm 50^\circ \text{C}$  and a water vapor  
partial pressure of  $> 200 \text{ mbar}$ . The oxygen partial  
pressure is set at a level that is compatible with the Cu-  
30 containing electrodes, i.e. at which the metallic copper  
will not oxidize and at which the ceramic will not be

reduced. The adjustment of the oxygen partial pressure is accomplished by gettering the oxygen from the nitrogen atmosphere, which contains water vapor, on large Cu surfaces, or by adding hydrogen.

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To determine the optimal ceramic composition, for example the ratio of Ti/Zr that corresponds to the morphotropic phase boundary, or the most favorable concentration of copper, first a series of compact, disk-shaped ceramic bodies are produced by stacking multiple 40-  
10 to 50- $\mu$ m-thick green films one on top of another and laminating them. After sintering, the finished ceramic test samples are contacted on both sides and their electrical properties are measured.

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The electrical properties of the compact ceramic test samples in the variable composition series are listed in Tables 2 through 4. The electrical properties of actuators having copper-containing internal electrodes and an  
20 optimized ceramic composition are listed in Table 5.

Examples of the debinding process for the compact ceramic test samples may be found in Table 1, with the specification of the residual carbon content in the  
25 components produced. The saturation temperature for water vapor in the debinding program is 97° C.

Table 1: Debinding of Compact Ceramic Test Samples (MLP [multilayer printed boards]) and the Corresponding  
30 Multilayer Ceramic Components (Actuators)

Conditions: R Ramp, H Holding Time	Test Samples	Residual Carbon Content Achieved C
R: 6.5 K/h $\Rightarrow$ 100° C, R: 6.2 K/h $\Rightarrow$ 220° C, R: 5 K/h $\Rightarrow$ 350° C, R: 15K/h $\Rightarrow$ 580° C, H: 15 h R: 150K/h, Final: 25° C	Ceramic samples MLP	220 ppm
	Actuators with 338 Cu Electrodes	184 ppm

According to the described decarbonization process and the indicated residual carbon content, in the subsequent sintering process at ca. 1000° C a densification of the ceramic of > 97% of the theoretic density occurs, without  
5 any damaging reductive degradation.

To allow the measurement of dielectric properties a gold electrode was applied to each side of the ceramic MLP  
10 test samples by means of vapor deposition.

In Table 2 the properties of compact ceramic test samples made from foils  $Pb_{1-3x/2-y/2}Se_x□_{x/2-y/2}Cu_y(Zr_{0.5515-z}Ti_{0.4485+z})O_3$  with  $Nd_2O_3$  as the dopant and  $x = 0.02$ , without a  
15 copper oxide additive ( $y = 0$ ) are compiled, wherein the Zr/Ti ratio for the test samples was varied. The production took place in an  $N_2$  atmosphere at a residual

oxygen partial pressure of  $p_{O_2} = 10^{-2} - 10^{-3}$  Pa, which was established using the partial pressure for water vapor  $p_{H_2O}$  and the hydrogen partial pressure  $p_{H_2}$ . Measurements were taken after polarization with  $E = 2$  kV/mm, at room  
5 temperature.

Table 2. Properties of Compact, Square Ceramic MLP Test Samples (side length  $a = 11.5$  mm, thickness  $h = 1$  mm) in the  $Pb_{0.97}Nd_{0.02}\square_{0.01}(Zr_{0.5515-z}Ti_{0.4485+z})O_3$  Series, for the  
10 Purpose of Determining the Morphotropic Phase Boundary, with Indication of Average Statistical Error, for 5 to 10 Individual Test Samples.

z	Dielectric Constant $\epsilon$	Temperature Coefficient $TK\epsilon$	Piezoelectric Load Constant $D_{33}$ [pm V <sup>-1</sup> ]	Density $P$ [g cm <sup>-3</sup> ]
0	$1339 \pm 9$	$6037 \pm 225$	$720 \pm 5$	$7.76 \pm 0.04$
0.0025	$1360 \pm 23$	$4985 \pm 91$	$728 \pm 12$	$7.54 \pm 0.10$
0.005	$1330 \pm 15$	$5094 \pm 150$	$723 \pm 8$	$7.59 \pm 0.02$
0.009	$1527 \pm 28$	$3913 \pm 247$	$753 \pm 14$	$7.89 \pm 0.02$
0.0125	$1436 \pm 74$	$3083 \pm 265$	$714 \pm 40$	$7.90 \pm 0.02$
0.0205	$1598 \pm 21$	$2740 \pm 110$	$707 \pm 20$	$7.88 \pm$

				0.02
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As is shown in the table, the small signal dielectric constant  $\epsilon$  increases and the temperature coefficient  $TK\epsilon$  decreases with the variation of the z-value, while the  $d_{33}$  value reaches a maximum level at  $z=0.009$ . Accordingly, the formula  $Pb_{0.97}Nd_{0.02}\square_{0.01}(Zr_{0.5425}Ti_{0.4575})O_3$  corresponds to a ceramic mass that is tailored to the morphotropic phase boundary for a preparation without added CuO.

In Table 3 the properties of compact ceramic test samples produced from foils and having the composition  $Pb_{1-3x/2-y/2}SE_x\square_{x/2-y/2}Cu_y(Zr_{0.5515-z}Ti_{0.4485+z})O_3$  with  $Nd_2O_3$  as the dopant and  $x = 0.02$  and  $z = 0$  are compiled, wherein the copper content was varied with the parameter y and in one case (in which  $y = 0.04$ ) exceeds the upper limit for homogeneous solubility in the perovskite lattice structure that is defined by  $x = y$ . The test samples were produced under  $N_2$  at a residual oxygen partial pressure of  $p_{O_2} = 10^{-2} - 10^{-3}$  Pa, established using  $p_{H_2O}$  and  $p_{H_2}$ . Measurements were taken following polarization with  $E = 2$  kV/mm, at room temperature.

Table 3. Properties of Compact, Square Ceramic MLP Test Samples (side length  $a = 11.5$  mm, thickness  $h = 1$  mm) in the  $Pb_{0.97-y/2}Nd_{0.02}Cu_y(Zr_{0.5515}Ti_{0.4485})O_3$  Series, for the Purpose of Determining an Optimal Copper Content, with Indication of Average Statistical Error, for 5 to 10 Individual Test Samples.

y	Dielectric Constant $\epsilon$	Temperature Coefficient TK $\epsilon$	Piezoelectric Load Constant $d_{33}$ [pm V <sup>-1</sup> ]	Density p [g cm <sup>-3</sup> ]
0	1339 $\pm$ 9	6037 $\pm$ 225	720 $\pm$ 5	7.76 $\pm$ 0.04
0.005	1125 $\pm$ 6	4202 $\pm$ 19	645 $\pm$ 6	7.78 $\pm$ 0.03
0.010	1100 $\pm$ 21	3466 $\pm$ 136	540 $\pm$ 11	7.58 $\pm$ 0.11
0.020	1317 $\pm$ 11	4107 $\pm$ 105	739 $\pm$ 4	7.71 $\pm$ 0.03
0.040	1151 $\pm$ 16	4112 $\pm$ 406	641 $\pm$ 11	7.93 $\pm$ 0.11

The values listed in the table indicate that the ceramic composition in which  $y = 0.02$  corresponds to an optimal copper content.

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In keeping with the above process, in Table 4 the ratio Zr/Ti was again varied, in order to determine the morphotropic phase boundary for a Cu content of  $y = 0.02$ .

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Table 4. Properties of Compact, Square Ceramic MLP Test Samples (side length  $a = 11.5$  mm, thickness  $h = 1$  mm) in the  $\text{Pb}_{0.96}\text{Nd}_{0.02}\text{Cu}_{0.02}(\text{Zr}_{0.5515-z}\text{Ti}_{0.4485+z})\text{O}_3$  Series, for the Purpose of Determining the Morphotropic Phase Boundary, with Indication of Average Statistical Error, for 5 to 10 Individual Test Samples.

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z	Dielectric	Temperature	Piezoelectric	Density
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	Constant $\epsilon$	Coefficient $TK\epsilon$	Load Constant $d_{33}$ [pm V <sup>-1</sup> ]	$p$ [g cm <sup>-3</sup> ]
-0.016	1005 $\pm$ 13	4970 $\pm$ 52	500 $\pm$ 6	7.40 $\pm$ 0.03
-0.008	1037 $\pm$ 15	4484 $\pm$ 207	454 $\pm$ 9	7.40 $\pm$ 0.03
0	1317 $\pm$ 1	4107 $\pm$ 105	739 $\pm$ 4	7.71 $\pm$ 0.03
0.009	1208 $\pm$ 32	3717 $\pm$ 58	581 $\pm$ 26	7.88 $\pm$ 0.02
0.0125	1214 $\pm$ 37	3707 $\pm$ 67	566 $\pm$ 11	7.89 $\pm$ 0.03
0.0205	1226 $\pm$ 39	3380 $\pm$ 115	513 $\pm$ 18	7.90 $\pm$ 0.02

It has been found that with the apparently optimal Cu content of  $y = 0.02$ , which is controlled by the SE cation content, in this case  $Nd^{3+}$ , the best value for the piezoelectric load constant  $d_{33}$  is again at a value of  $z = 0$ , in other words with the insertion of  $Cu^+$  ions in place of  $Ag^+$  ions, the morphotropic phase boundary is established at approximately equal concentrations of Ti and Zr, i.e. at a Zr/Ti ratio of approximately 1.

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Multilayer piezoelectric components (actuators), for example piezo stacks having several hundred copper-containing internal electrodes, that are based upon the ceramic masses of the invention, are produced according to standard methods of printing the ceramic layers with a

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copper paste, stacking the printed ceramic layers,  
laminating them, debinding them, and sintering them.

In Table 5 the properties of three actuators having  
5 the different ceramic compositions

1)  $\text{Pb}_{0.97}\text{Nd}_{0.02}\square_{0.01}(\text{Zr}_{0.5515}\text{Ti}_{0.4485})\text{O}_3$  without  
adjustment for Cu internal electrodes;

2)  $\text{Pb}_{0.97}\text{Nd}_{0.02}\square_{0.01}(\text{Zr}_{0.5425}\text{Ti}_{0.4575})\text{O}_3$  with adjustment  
of the Zr/Ti ratio for Cu internal electrodes;

10 3)  $\text{Pb}_{0.96}\text{Nd}_{0.02}\text{Cu}_{0.02}(\text{Zr}_{0.5515}\text{Ti}_{0.4485})$  with a Cu  
content tailored to the dopant and established  
morphotropic phase boundary,

each with 360 internal electrodes and a ceramic layer  
thickness of 80  $\mu\text{m}$  are compiled, with measurements being  
15 taken after a polarization with  $E = 2 \text{ kV/mm}$ , (a) at room  
temperature and (b) at  $180^\circ \text{ C}$ . In addition to the small-  
signal properties  $\epsilon$  and  $\text{TK}\epsilon$ , in this case the large-signal  
dielectric constant is also indicated, which can be  
calculated from the polarization using a voltage, which for  
20 example in the actuators results in a deflection of 40  $\mu\text{m}$ .

Table 5: Properties of Actuators with Copper-  
Containing Internal Electrodes Based Upon the Ceramic

25 1)  $\text{Pb}_{0.97}\text{Nd}_{0.02}\square_{0.01}(\text{Zr}_{0.5515}\text{Ti}_{0.4485})\text{O}_3$  without the  
addition of copper oxide and without adjustment for  
the morphotropic phase boundary,

2)  $\text{Pb}_{0.97}\text{Nd}_{0.02}\square_{0.01}(\text{Zr}_{0.5425}\text{Ti}_{0.4575})\text{O}_3$  with adjustment  
of the Zr/Ti ratio to the morphotropic phase boundary,  
and



- 3) a ceramic  $\text{Pb}_{0.96}\text{Nd}_{0.02}\text{Cu}_{0.02}(\text{Zr}_{0.5515}\text{Ti}_{0.4485})$ ,  
modified by the addition of copper oxide,  
the Zr/Ti ratio of which is tailored to the  
morphotropic phase boundary. Measurements were taken  
5 following a polarization with 2 kV/mm (a) at room  
temperature and (b) at 180° C.

z	Dielectric Constant		Temperature Coefficient	Piezoel. Load Constant	Efficiency Level $\eta$	Dielectric Loss Energy L [mJ]
	Small Signal	Large Signal	TK $\epsilon$ (small signal)	$d_{33}$ [pm V <sup>-1</sup> ]		
(1)	1214±30	3110±87	3936±82	592 ± 18	50.4 ± 0.4	50 ± 2
(a)						
(b)		2772±50		632 ± 11	56.5±0.4	34 ± 1
(2)	1358±27	2984±118	2949±41	568 ± 15	51±0.7	51 ± 2
(a)						
(b)		2841±57		614 ± 11	57± 1	37 ± 2
(3)	1216±8	2747±102	2860±42	569 ± 11	55± 1	44 ± 1
(a)						

- From the figures listed in Table 5, a comparison of  
10 the actuators containing the two ceramics (1) and (2) shows  
an improvement in properties in terms of a reduction in the  
TK $\epsilon$  in the ceramic 2a relative to the ceramic 1a. However a  
significant reduction in the dielectric loss energy L  
results only with the insertion of copper. At 44 mJ, the  
15 value for the dielectric loss L for the ceramic (3) with  
polarization at room temperature lies well below the values  
for those actuators that were produced using the ceramic

without copper oxide additive. A further improvement can be achieved with thermal polarization at, for example, 180° C. In addition, in this case the dependence of the small-signal capacitance on the temperature is lower.

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Although the invention has been detailed using only a small number of exemplary embodiments, it can be used to produce ceramic materials having any values for the parameters x, y and z. In principle, other raw material masses and copper additives or additives containing copper oxide that are not mentioned here but are suitable for producing the ceramic of the indicated general composition can also be used. Suitable raw material masses are known, for example, from the publication DE 20023051 U1.

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